

## Recent advances of quartz-enhanced photoacoustic spectroscopy sensor technology

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Quartz-enhanced photoacoustic spectroscopy (QEPAS) sensor technology is based on a new approach to photoacoustic detection which employs a quartz tuning fork (TF) as a resonant acoustic transducer [1,2]. A QEPAS sensor detects the weak acoustic pressure wave that is generated when optical radiation interacts with a trace gas. The weak pressure wave excites a resonant vibration of a TF which is then converted into an electric signal by the piezoelectric effect. Subsequently, the electric signal, which is proportional to the concentration of the gas, is measured by a transimpedance amplifier. Merits of QEPAS compared to conventional resonant photoacoustic spectroscopy include QEPAS sensor immunity to environmental acoustic noise, a simple absorption detection module design, and its capability to analyze trace gas samples of  $\sim 1 \text{ mm}^3$  in volume.

This poster reports recent improvements of spectrophone design and QEPAS based sensor performance. In order to enhance the amplitude of the photoacoustic signal, it is advantageous to place a TF within a microresonator composed of two thin tubes, so that the microresonator yields a signal gain from 10 to 20. To-date, we have investigated the sensor performance with  $l=4\text{mm}$ ,  $4.4\text{mm}$  and  $5\text{mm}$  long metal tubes with ID= $0.4 \text{ mm}$ ,  $0.5 \text{ mm}$ ,  $0.58 \text{ mm}$ ,  $0.6 \text{ mm}$ ,  $0.76 \text{ mm}$  and  $0.084 \text{ mm}$ . A near-infrared fiber-coupled distributed feedback (DFB) diode laser (JDS Uniphase model CQF935/908-19600) was used as the QEPAS excitation source. The diode laser output was split into a 1:99 ratio by means of a fiber beam splitter (ThorLabs 10202A-99-APC). A small fraction of the laser light was sent to a commercial fiber-coupled reference gas module (Wavelength References, Mulino, OR) containing a sealed cell filled with a mixture of 5 Torr  $\text{C}_2\text{H}_2$  and 145 Torr  $\text{N}_2$ , a fiber collimator, and a photodiode. The remaining laser power was directed to a spectrophone consisting of the TF and two tubes forming the acoustic microresonator. The spectrophone was placed into a vacuum-tight enclosure (the inner gas volume is  $V \sim 1 \text{ cm}^3$  when the spectrophone is installed) equipped with two sapphire windows and gas inlet and outlet.  $\text{C}_2\text{H}_2$  in  $\text{N}_2$  (10 ppmv) was used as a convenient target gas whose flow was set to 100 ccm. A control electronics unit was employed to measure the  $f_{\text{TF}}$  and  $Q$ -factor of the TF, to modulate the laser current at  $f_L = 1/2 f_{\text{TF}}$ , to lock the laser wavelength to the targeted absorption line and to measure the current generated by the TF in response to the photoacoustic signal. For a specific length tube configuration, we varied the gas pressures by means of a pressure controller (MKS Type 649) to obtain signal amplitudes for different gas pressures.

The sensor performance was evaluated based on the SNR with a calibrated  $\text{C}_2\text{H}_2$  gas mixture. In Ref. [3] it was shown that the TF noise is inversely proportional to the square root of the equivalent resistor  $R$  of the TF. Therefore, the SNR is proportional to the product of signal amplitude and  $\sqrt{R}$  of the TF. The optimal microresonator parameters are  $l=4.4\text{mm}$  and ID= $0.5\text{mm}$ , with the two gaps between TF and the microresonator tubes set to between  $30\mu\text{m}$  and  $50\mu\text{m}$ .

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